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Computer code for the optimization of performance parameters of mixed explosive formulations

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Abstract

LOTUSES is a novel computer code, which has been developed for the prediction of various thermodynamic properties such as heat of formation, heat of explosion, volume of explosion gaseous products and other related performance parameters. In this paper, we report LOTUSES (Version 1.4) code which has been utilized for the optimization of various high explosives in different combinations to obtain maximum possible velocity of detonation. LOTUSES (Version 1.4) code will vary the composition of mixed explosives automatically in the range of 1–100% and computes the oxygen balance as well as the velocity of detonation for various compositions in preset steps. Further, the code suggests the compositions for which least oxygen balance and the higher velocity of detonation could be achieved. Presently, the code can be applied for two component explosive compositions. The code has been validated with well-known explosives like, TNT, HNS, HNF, TATB, RDX, HMX, AN, DNA, CL-20 and TNAZ in different combinations. The new algorithm incorporated in LOTUSES (Version 1.4) enhances the efficiency and makes it a more powerful tool for the scientists/researches working in the field of high energy materials/hazardous materials.

Keywords: Mixed explosives; Velocity of detonation; Oxygen balance; Explosive formulations; Modelling; Hazardous materials

1. Introduction

The study of energetic systems by theoretical methods has accelerated dramatically over the course of the last two decades and has proved considerable insight into the understanding of energetic materials [1–5]. The ability to predict the performance parameters of new explosive formulation is very much useful before one undertakes the laborious and expensive process of synthesising/formulating the same. Rigorous theoretical and mathematical approaches developed at present allow us to formalize the knowledge of specialists in formulation of mixed explosive composition. Most explosive and propellant compositions contain a mixture of components to have a maximum performance. Some of the components may not contribute to the heat liberated and may not even contain oxygen. These materials may however, contribute to the gaseous products and reduce

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the actual temperatures obtained on detonation of the explosive or burning of the propellant. For example, the explosive amatol contains mixtures of ammonium nitrate and TNT. Ammonium nitrate has an oxygen balance of +20% and TNT has an oxygen balance of -74%, so it would appear that the mixture yielding an oxygen balance of zero would also result in the best explosive properties. In actual practice a mixture of 80% ammonium nitrate and 20% TNT by weight yields an oxygen balance of +1%, and shows an increase in strength of 30% over TNT.

Computation to get maximum performance properties of mixed explosive composition by repeated iteration calls for tedious calculation. A new algorithm developed by authors is time saving as well as accurate for the prediction of performance parameters of mixed explosive composition and it is successfully incorporated with LOTUSES code. LOTUSES also can predict the velocity of detonation, density, C–J pressure, heat of explosion, heat of formation, volume of explosion of gaseous products, etc. [6–10]. The new algorithm incorporated enhances its efficiency and allow theoretical screening of notional hazardous materials for identification of promising mixed explosive composition for additional study and elimination of weaker can-

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didates from further consideration. Thereby, reduces the cost associated with the development programme of the high energy materials as well as reduces the duration of development programme. In this paper, we report the velocity of detonation and oxygen balance of mixed explosive formulations computed by LOTUSES (Version 1.4) at different compositions in brief.

Thermochemical/hydrodynamic computer codes such as BKW (Charles L. Mader, first in 1956 for IBM 704, STRETCH BKW in 1961 for IBM 7030, using Fortran IV BKW in 1967) [11-14], RUBY [15], TIGER [16,17], PANDA [18], CHEQ code [19], and CHEETAH [20] have been reported in literature for the prediction of various thermodynamic as well as detonation parameters. But these codes does not gives automatically the optimum composition corresponds to maximum detonation velocity and minimum oxygen balance of mixed explosive formulations. Hence, a new algorithm incorporated in LOTUSES-1.4, which automatically varies the composition of mixed explosive formulations and gives the optimum composition corresponds to maximum detonation velocity and minimum oxygen balance will be of immense value for the scientists, academicians and technologists working in the field of HEMs for designing high performance mixed explosive formulations.

2. Computation of HEMs parameter

2.1. Evaluating oxygen balance

Oxygen balance (OB) of an explosive is a highly important parameter to decide its performance and is defined as the percentage excess/deficiency of oxygen in the explosive molecule to completely oxidize carbon, hydrogen to CO_2 and H_2O , respectively. It is observed that the heat of explosion reaches a maximum for an oxygen balance of zero, since this corresponds to the stoichiometric oxidation of carbon to carbon dioxide and hydrogen to water. The oxygen balance can therefore be used to optimize the composition of the explosive to give an oxygen balance as close to zero as possible [21,22].

The oxygen balance provides information about the types of gases liberated during explosion. If the oxygen balance is large and negative then there is not enough oxygen for carbon dioxide to be formed. Consequently, toxic gases such as carbon monoxide will be liberated. This is very important for commercial explosives as the amount of toxic gases liberated must be kept to a minimum. Explosives for use underground with poor ventilation should be formulated to produce a minimum total toxic effect. The molecule is said to have a positive oxygen balance if it contains more oxygen than is needed. An explosive with excess oxygen produces toxic NO and NO₂. Commercial explosives are usually close to oxygen-balanced, so that the main detonation products are water, carbon dioxide, and nitrogen. The sensitivity, strength and brisance of an explosive are all somewhat dependent upon oxygen balance and tend to approach their maximum as oxygen balance approaches zero. The limitation of OB it that, OB does not provide information on the energy changes which take place during an explosion.

The oxygen balance (OB) is calculated from the empirical formula of a compound in percentage of oxygen required for



Fig. 1. VOD vs. % composition of AN with TNT.



Fig. 2. VOD vs. OB of AN with TNT.

complete conversion of carbon to carbon dioxide, hydrogen to water and metal to metal oxide. The procedure for calculating oxygen balance in terms of 100 g of the explosive material is to determine the number of gram atoms of oxygen that are excess or deficient for 100 g of a compound. A quantitative measure of oxygen balance can be defined as

$$OB = \frac{-100 \times MW(O) \times [2C + H/2 + M-O]}{MW(explosive)}$$

where C, H, M and O are the number of carbon, hydrogen, metal and oxygen in a molecule, MW(O) is the molecular weight of oxygen (=16 g/mol) and MW(explosive) is the molecular weight of explosive.

2.2. Velocity of detonation

Velocity of detonation (VOD) is the rate of propagation of the explosive reaction through the explosive material [23]. Detonation is a form of reaction given by an explosive substance in which the chemical reaction produces a shock wave. High temperature and pressure gradients are generated in the wave front, so that the chemical reaction is initiated instantaneously. Knowledge of the detonation velocity is important because it is the easiest of the C–J state parameters to measure accurately and used to determine all of the other C–J state parameters [24]. A number of attempts have been made over the last few decades to theoretically predict the VOD of explosives [25–36]. In the present work, we have used the Rothstein et al. method [25,26] for the computation of velocity of detonation of mixed explosive composition to get the maximum performance.

Table 1
Velocity of detonation (VOD) and oxygen balance (OB) of mixed explosive composition predicted by LOTUSES Version 1.4

S. no.	Compound	Molecular formula	Computation by LOTUSES 1.4				
			%	Mixed composition	OB (%)	VOD (km/s)	
1	RDX	$C_3H_6N_6O_6$	90	$C_{1.52361}H_{2.65101}N_{2.56296}O_{2.69503}$	-26.84	8.799	
	TNT	$C_7H_5N_3O_6$	10				
2	RDX	$C_3H_6N_6O_6$	80	$C_{1.6967}H_{2.60103}N_{2.4249}O_{2.68908}$	-32.0	8.552	
	TNT	$C_7H_5N_3O_6$	20				
3	RDX	$C_3H_6N_6O_6$	70	$C_{1.8698}H_{2.55105}N_{2.2869}O_{2.68313}$	-37.31	8.305	
	TNT	$C_7H_5N_3O_6$	30				
4	HMX	$C_4H_8N_8O_8$	90	$C_{1.52361}H_{2.65101}N_{2.56296}O_{2.69503}$	-26.84	8.799	
	TNT	$C_7H_5N_3O_6$	10				
5	HMX	$C_4H_8N_8O_8$	80	$C_{1.69673}H_{2.60103}N_{2.42493}O_{2.68908}$	-32.07	8.552	
	TNT	$C_7H_5N_3O_6$	20				
6	HMX	$C_4H_8N_8O_8$	70	C _{1.86985} H _{2.55105} N _{2.28691} O _{2.68313}	-37.31	8.305	
	TNT	$C_7H_5N_3O_6$	30				
7	ONC	$C_8N_8O_{16}$	90	C _{1.85933} H.26662N _{1.68323} O _{3.36647}	-7.76	9.238	
	TNT	$C_7H_5N_3O_6$	10				
8	ONC	$C_8N_8O_{16}$	80	C _{1.99515} H _{.52663} N _{1.64295} O _{3.28591}	-15.46	8.941	
	TNT	$C_7H_5N_3O_6$	20				
9	ONC	$C_8N_8O_{16}$	70	C _{2.13097} H _{.77335} N _{1.60267} O _{3.20535}	-23.06	8.645	
	TNT	C7H5N3O6	30				
10	TATB	$C_6H_6N_6O_6$	90	C _{2 09161} H _{2 5912} N _{2 34145} O _{2 46637}	-48.20	7.919	
	AN	$H_4N_2O_3$	10	2.07101 2.0712 2.04140 2.40007			
11	TATB	C ₆ H ₆ N ₆ O ₆	80	C1 85921H2 85856N2 35888O2 6087	-40.62	8.169	
	AN	$H_4N_2O_3$	20	-1.057212.050502.050602.0007			
12	TATB	CeHeNeOe	70	C1 6268 H2 12582 N2 27622 O2 75108	-33.04	8 422	
	AN	$H_4N_2O_3$	30	01.0206113.12363112.37032 02.73108	00101	01122	
13	TNT	$C_7H_5N_2O_6$	90	C2 77252H2 4807N1 42840O2 75207	-64.56	6 933	
	AN	$H_4N_2O_3$	10	2.77333×2.4807×1.43849 2.73207	01100	0.700	
14	TNT	$C_7H_5N_2O_6$	80	C2 46526 H2 7602 N1 5562 O2 8626	-55.17	7 291	
11	AN	$H_4N_2O_2$	20	02.40330112.70031 (1.3302 02.8020	55.17	1.291	
15	TNT	$C_7H_5N_2O_6$	20 70	C2 1571 H2 0208 N1 67402 O2 07220	-45 77	7 653	
15	AN	$H_4N_2O_2$	30	02.13/1113.03981 (1.8/402 02.9/529	13.77	1.055	
16	HNS	$C_{14}HeNeO_{12}$	90	C2 70827 H1 60807 N1 44014 O2 77226	-58 76	7 253	
10	AN	$H_4N_2O_2$	10	02./963/111.0989/111.44914 02.//550	56.76	1.200	
17	HNS	CitHeNcOia	80	C2 49744 H2 06520 N1 5657 O2 9916	-50.01	7 567	
17	AN	$H_4N_2O_2$	20	02.48744112.00539111.5057 02.8816	50.01	1.501	
18	HNS	$C_1 + H_2 N_2 O_{12}$	20 70	Co 17671 Ho 10101 N1 6000 Op 00005	-41.26	7 888	
10	AN	$H_4N_2O_2$	30	C2.1/651112.43181111.6823 C2.98985	-41.20	7.000	
19	CL-20	C(H(N))2O12	90	C1 5402 H1 45224 N2 50(51 O2 72858	-17.25	9 331	
1)	TNT	$C_7H_5N_2O_6$	10	01.3403111.452341 02.39051 02.72838	17.25	2.551	
20	CL-20	CeHeNiaOia	80	Current Hugars No 45475 Op 7100	_23 55	9.026	
20	TNT	$C_{2}H_{2}N_{2}O_{12}$	20	C1./1164111.53551 2.454/5 C2./189	-23.55	9.020	
21	CL-20	C H N 10 O 10	20	C1 0000 H1 01075 No 210 Oo 70000	_29.85	8 721	
21	TNT	$C_{7}H_{7}N_{2}O_{7}$	30	C1.8829111.618751 (2.315 C2.70922	27.05	0.721	
22	CL-20	C(H(N)aO)a	90	Ci accas Hi ucua Na czacz Oa zacze	_11.52	8 963	
22	TNAZ	$C_{2}H_{4}N_{4}O_{5}$	10	01.38838111.440431 2.6/203 02.7/6/6	11.52	0.905	
23	CL_{20}	$C_{14}N_{4}O_{6}$	80	Course House Na corres Oa auro	_12.09	8 807	
25	TNAZ	$C_{0}H_{1}N_{1}O_{1}$	20	C1.40/63111.511/41 2.60/05 C2.8152	-12.07	0.077	
24	CL 20	$C_{3}H_{4}N_{4}O_{6}$	20	C	12.66	8 837	
24	CL-20 TNAZ	$C_{6}H_{6}N_{12}O_{12}$	20	C1.42688111.583051 2.54144 C2.85377	-12.00	0.052	
25	TEV	$C_{1}H_{1}N_{1}O_{2}$	30	C H N O	40.11	7 806	
23	TEA TNAZ	$C_6H_6N_4O_8$	90	C2.21602H2.26807IN1.58145O3.058809	-40.11	7.890	
26	TEX	$C_3H_4N_4O_6$	10	C II N O	27.50	9.017	
20	IEA TNAZ	$C_{6}H_{6}N_{4}O_{8}$	80 20	C _{2.14331} H _{2.24742} N _{1.63709} O _{3.06597}	-57.50	8.017	
27	TEX	$C_3H_4N_4O_6$	20	C II N O	24.00	9 120	
27	IEA TNA 7	$C_6H_6N_4O_8$	70	C _{2.070607} H _{2.226772} N _{1.69273} O _{3.073139}	-34.90	8.139	
20	TEV	$C_3 \Pi_4 N_4 O_6$	50		15 04	7 655	
28	IEX	$C_6H_6N_4O_8$	90	C2.36803H2.27998N1.50531O3.01062	-45.84	/.055	
20	INT	$C_7H_5N_3O_6$	10		40.07	7.506	
29	TEX	$C_6H_6N_4O_8$	80	C2.44732H2.2712N1.4848O2.969608	-48.97	1.536	
	TNT	$C_7H_5N_3O_6$	20				
30	TEX	$C_6H_6N_4O_8$	70	$C_{2.52662}H_{2.26247}N_{1.46429}O_{2.9285}$	-52.09	7.418	
	TNT	$C_7H_5N_3O_6$	30				
31	ONC	C ₈ N ₈ O ₁₆	90	$C_{1.90443}H_{.36678}N_{1.65209}O_{3.35466}$	-10.19	9.130	
	DNA	$C_7H_6N_2O_5$	10				

Table 1 (Continued)

S. no.	Compound	d Molecular formula	Computation by LOTUSES 1.4				
			%	Mixed composition	OB (%)	VOD (km/s)	
32	ONC	$C_8N_8O_{16}$	80	$C_{2.08536}H_{.72446}N_{1.58068}O_{3.26230}$	-20.30	8.725	
	DNA	$C_7H_6N_2O_5$	20				
33	ONC	$C_8N_8O_{16}$	70	$C_{2.26629}H_{1.06386}N_{1.50926}O_{3.1699}$	-30.26	8.322	
	DNA	$C_7H_6N_2O_5$	30				
34	CL-20	$C_6H_6N_{12}O_{12}$	90	$C_{1.58549}H_{1.53502}N_{2.56537}O_{2.71677}$	-19.54	9.22	
	DNA	$C_7H_6N_2O_5$	10				
35	CL-20	$C_6H_6N_{12}O_{12}$	80	$C_{2.01822}H_{1.86681}N_{2.21959}O_{2.67380}$	-28.14	8.810	
	DNA	$C_7H_6N_2O_5$	20				
36	CL-20	$C_6H_6N_{12}O_{12}$	70	$C_{1.8018}H_{1.70092}N_{2.39248}O_{2.69529}$	-36.73	8.395	
	DNA	$C_7H_6N_2O_5$	30	a w w a	50.00	= 150	
37	TATB	$C_6H_6N_6O_6$	90	$C_{2.4448}H_{2.39442}N_{2.1925}O_{2.34395}$	-59.88	7.452	
	DNA	$C_7H_6N_2O_5$	10	a w w a	< 1.00	= = = =	
38	TATB	$C_6H_6N_6O_6$	80	$C_{2.56576}H_{2.4648}N_{2.06108}O_{2.36389}$	-64.00	7.230	
20	DNA	$C_7H_6N_2O_5$	20		(0.11	7 000	
39	TAIB	$C_6H_6N_6O_6$	70	$C_{2.68664}H_{2.5352}N_{1.9296}O_{2.38383}$	-68.11	7.009	
40	DNA	$C_7H_6N_2O_5$	30	C U N O	20.12	9 (90	
40	HMX	$C_4H_8N_8O_8$	90	C _{1.56872} H _{2.73369} N _{2.5318} O _{2.68323}	-29.13	8.689	
41	DINA	$C_7 H_6 N_2 O_5$	10	C II N O	26.66	0 221	
41		$C_4 \Pi_8 N_8 O_8$	20	C1.7869 I 2.7664 N 2.3626 C 2.66547	-30.00	6.551	
42	HMY	$C_7 H_6 N_2 O_5$	20	Conserve House No conserve On current	44 10	7 074	
42	DNA	C=H_N=O=	70 30	C2.0051/112./99111 2.193502 C2.647/1	-44.19	1.974	
43	RDX	$C_{2}H_{2}N_{2}O_{5}$	90	C1 56972H2 72260N2 52192O2 69222	-29.13	8 689	
	DNA	$C_{7}H_{c}N_{2}O_{5}$	10	01.308/2112./33091 02.33182 02.08323	27.15	0.009	
44	RDX	$C_2H_6N_2O_5$	80	C1 7860 H2 766400 N2 26266 O2 66547	-36.66	8 331	
	DNA	$C_7H_6N_2O_5$	20	01.7809112.700409112.30200 02.00347	50.00	0.551	
45	RDX	$C_2H_6N_6O_6$	20 70	C2 00517H2 700110N2 102501O2 64771	-44.19	7.974	
ч <i>3</i>	DNA	$C_7H_6N_2O_5$	30	-2.003172.799119- 2.193301 - 2.04771			
46	ONC	$C_8N_8O_{16}$	90	C1 70732H 25221N1 75938O3 41465	-2.01	9.469	
	TNAZ	$C_3H_4N_4O_6$	10	- 1.10152 - 1.5221 - 1.15550 - 5.41405			
47	ONC	$C_8N_8O_{16}$	80	C1.69114H.498159N1.79525O3.38228	-3.98	9.404	
	TNAZ	$C_3H_4N_4O_6$	20				
48	ONC	$C_8N_8O_{16}$	70	C _{1.67495} H _{.73154} N _{1.83111} O _{3.3499}	-5.84	9.344	
	TNAZ	$C_3H_4N_4O_6$	30				
49	HNS	$C_{14}H_6N_6O_{12}$	90	$C_{2.95453}H_{1.40752}N_{1.40752}O_{2.710934}$	-62.43	7.149	
	TNAZ	$C_3H_4N_4O_6$	10				
50	HNS	$C_{14}H_6N_6O_{12}$	80	$C_{2.79977}H_{1.48248}N_{1.482486}O_{2.756751}$	-57.34	7.352	
	TNAZ	$C_3H_4N_4O_6$	20				
51	HNS	$C_{14}H_6N_6O_{12}$	70	$C_{2.645005}H_{1.557449}N_{1.5574}O_{2.80256}$	-52.25	7.555	
	TNAZ	$C_3H_4N_4O_6$	30				
52	TATB	$C_6H_6N_6O_6$	90	$C_{2.247779}H_{2.29983}N_{2.29983}O_{2.40394}$	-51.86	7.815	
	TNAZ	$C_3H_4N_4O_6$	10				
53	TATB	$C_6H_6N_6O_6$	80	$C_{2.17154}H_{2.27565}N_{2.27565}O_{2.48387}$	-47.95	7.954	
	TNAZ	$C_3H_4N_4O_6$	20				
54	TATB	$C_6H_6N_6O_6$	70	C _{2.095305} H _{2.25147} N _{2.25147} O _{2.56379}	-44.04	8.090	
~ ~	TNAZ	$C_3H_4N_4O_6$	30		26.04	0.700	
22	FOX-/	$C_2H_4N_4O_4$	90	C _{1.523616} H _{2.65101} N _{2.56296} O _{2.69503}	-26.84	8.799	
57	INI EOV 7	$C_7H_5N_3O_6$	10	C U N O	22.07	0 550	
56	FUA-7 TNT	$C_2H_4N_4O_4$	20	C1.69673 T 2.60103 N 2.42493 C 2.68908	-32.07	8.332	
57	FOX 7	$C_7 H_5 N_3 O_6$	20	Ci acosco Ha conor Na acosci Oa coast	_37.31	8 305	
51	TNT	CaHaNaOa	30	C1.869858112.551051N2.28691 C2.68313	-57.51	0.505	
58	FOX-7	$C_{2}H_{2}N_{2}O_{6}$	<u>00</u>	Ci come Ha marce Na marce On serve	_20.13	8 680	
50	DNA	$C_2 H_4 N_4 O_4$	10	C1.56872**2.73369**2.53182*C2.68323	-27.13	0.007	
59	FOX-7	$C_{2}H_{4}N_{4}O_{4}$	80	C1 7000 Ha 7000 Na acases Oa cora	-36.66	8 331	
57	DNA	$C_2H_4N_4O_4$	20	C1./809++2./004++2.502004 C2.0054/	50.00	0.551	
60	FOX-7	$C_2H_4N_4O_4$	70	C2 00517 H2 700110 N2 102502 O2 64771	-44 19	7.974	
~ ~	DNA	$C_7H_6N_2O_5$	30	-2.005172.777117**2.175502~2.04//1			

 Table 2

 Abbreviation of explosives and their corresponding name, structure

S. no.	Name of the HEM	Abbreviation	Molecular formula	Structure	Velocity of detonation (km/s)		
					Literature	LOTUSES	Deviation
1	2,4,6-Trinitrotoluene	TNT	$C_7H_5N_3O_6$	O ₂ N NO ₂ NO ₂	6.9	6.66456	0.23544
2	<i>Trans-2,2',4,4',6,6'-</i> hexanitrostilbene	HNS	$C_{14}H_6N_6O_{12}$	O_2N O_2N O_2N C = C O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2N O_2	7.12	6.82942	0.29058
3	Octanitrocubane	ONC	$C_8N_8O_{16}$	O ₂ N O ₂ N O ₂ N O ₂ N NO ₂ NO ₂ NO ₂	9.9	9.0588	0.8412
4	1,3,5-Triamino-2,4,6- trinitrobenzene	TATB	$\mathrm{C_6H_6N_6O_6}$	$(O_2N) \xrightarrow{NH_2} NO_2$ $H_2N \xrightarrow{NO_2} NO_2$	7.94	7.86086	0.07914
5	Cyclotrimethylenetrinitramine	RDX	$C_3H_6N_6O_6$	O ₂ N N ₁ H ₂ C NO ₂ H ₂ C CH ₂ NO ₂	8.85	8.93981	-0.08981
6	Cyclotetramethyl- enetetranitramine	НМХ	$\mathrm{C_4H_8N_8O_8}$	NO_{2} $H_{2}C - N - CH_{2}$ $O_{2}N - N - NO_{2}$ $H_{2}C - N - CH_{2}$	9.1	9.04212	0.05788
7	Ammonium nitrate	AN	$H_4N_2O_3$	NO ₂ NH ₄ NO ₃	5.27	7.3442	-2.0742
8	Hexanitrohexa- azaisowurtzitane	CL-20	$C_6H_6N_{12}O_{12}$	O ₂ NN NNO ₂ O ₂ NN NNO ₂ NNO ₂	9.4	9.3808	0.0192
9	1,3,3-Trinitroazetidine	TNAZ	$C_{3}H_{4}N_{4}O_{6}$	^{O₂N, NO₂ NO₂}	8.5	8.6763	-0.1763

Table 2 (*Continued*)

S. no.	Name of the HEM	Abbreviation	Molecular formula	Structure	Velocity of detonation (km/s)		
					Literature	LOTUSES	Deviation
10	2,4-Dinitroanisole	DNA	C7H6N2O5	NO ₂	6.74	5.7057	1.0343
11	1,1-Diamino-2,2-dinitro- ethylene	FOX-7	C ₂ H ₄ N ₄ O ₄	$\underset{H_2N}{\overset{H_2N}{\longrightarrow}}\underset{NO_2}{\overset{NO_2}{\longrightarrow}}$	9.09	8.7351	0.3549
12	Tetraoxa explosive 4,10-dinitro-2,6,8,12- tetraoxa-4,10- diazatetracyclo-(5.5.0.05,9 03,11)dodecane	TEX	$\mathrm{C_6H_6N_4O_8}$	O ₂ N ^{-N} NO ₂	8.665	7.8210	0.844

3. Results and discussion

Computer code named LOTUSES-1.4 is developed to optimize the mixed explosive composition to get maximum output performance. The approach involved in the development of code comprises two important steps: (i) optimization of the oxygen balance of the ingredients and (ii) prediction of maximum possible detonation velocity for mixed explosive composition. The algorithm written in LOTUSES-1.4 by the author, vary the composition of mixed explosives automatically in the range of 1–100% and computes the oxygen balance as well as the velocity of detonation for various compositions in preset steps. At the end of several iterations performed by LOTUSES-1.4, it automatically gives the optimized composition of mixed explosive for which maximum output performance of mixed explosive is expected.

Most of the military explosives are solid compositions, which are made up of two explosive components. Generally two different techniques are followed to make military explosive compositions, namely: (i) melt casting and (ii) pressing. Explosive compositions which are processed by melt casting are generally contains TNT, which has a relatively low melting temperature (80 °C) compared with its ignition temperature (240 °C). In this paper, we report a variety of melt cast explosive formulations with their predicted performance properties at different compositions. The velocity of detonation and oxygen balance data generated by LOTUSES (Version 1.4) for high explosives like RDX, HMX, ONC, CL-20, TATB, HNS, TEX, FOX-7 with low melting ingredients like TNT, DNA and TNAZ at different compositions are presented in Table 1. The variation of velocity of detonation with increase in the composition of ammonium nitrate (AN) is shown in Fig. 1. The data in Fig. 1 shows that the velocity of detonation of mixed explosive is greater than the

individual component at 80:20 composition, which is confirmed by the reported in literature [23]. In Fig. 2, oxygen balance and velocity of detonation of AN:TNT mixture at different composition is plotted along X and Y axis, respectively. The results depicted in Fig. 2 and Table 1 reveals that, when the oxygen balance of mixed explosive composition approaches towards zero, their velocity of detonation increases. Abbreviation of explosives and their corresponding name, structures are given in Table 2. Also Table 2 presents the comparison of velocity of detonation for pure explosives generated using LOTUSES (Version 1.4) with reported in literatures [23,25,26,37–41].

4. Conclusion

An algorithm to compute the performance properties of mixed explosive composition is developed and successfully incorporated to the existing LOTUSES code. The computer code has been validated with well-known explosive RDX, HMX, ONC, CL-20, TATB, HNS, TEX, FOX-7 with low melting ingredients like TNT, DNA and TNAZ at different compositions. LOTUSES also can predict the velocity of detonation, density, C-J pressure, heat of explosion, heat of formation, volume of explosion of gaseous products, etc., the new algorithm incorporated enhances its efficiency and makes it a more powerful tool for the scientists/researches working in the field of high energy materials. Finally, it is concluded that the new algorithm incorporated in LOTUSES (Version 1.4) will allow theoretical screening of notional hazardous materials for identification of promising mixed explosive compositions for additional study and elimination of weaker candidates from further consideration. Thereby, reducing cost associated with the development programme of the high energy materials.

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